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16. Abstract FPS 19W is the approved flexible pavement thickness design system used by the Texas Department of Transportation (TxDOT). Project 0-1869 made several enhancements to this system, including: <ul style="list-style-type: none"> transferring the system to the Windows® platform, automating the Texas Triaxial system to provide a thickness checking system, incorporating stress and strain computational subsystem so that classical fatigue and rutting lives can be estimated for the designed pavement, and incorporating an extensive on-line help system. In this project the models within FPS 19W were further calibrated. New approaches were also incorporated for handling designs on pavements with very thick flexible bases.			
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FLEXIBLE PAVEMENT DESIGN SYSTEM FPS 19W: USER'S MANUAL

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DISCLAIMER

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CHAPTER 1

INTRODUCTION

FPS 19W is the mechanistic-empirical flexible pavement design program that has been in use by the Texas Department of Transportation (TxDOT) since the mid 1990s. The system was developed earlier under Project 7-1987, and details of the performance models can be found in an earlier report (1). The material property required to perform the pavement design is the modulus of each pavement layer. In Texas these values are backcalculated from Falling Weight Deflectometer (FWD) data using the MODULUS backcalculation system (2).

In Project 0-1869 a continuing effort was made to improve both the MODULUS and the FPS 19W design system. One objective was to develop new versions of the programs, which run under the Windows® environment. Substantial enhancements were made to FPS 19W including the addition of on-line design checking capabilities and the incorporation of a full linear elastic analysis package to compute stress and strains for the selected pavement structure. These additions were intended to provide TxDOT districts with tools to continue the implementation of mechanistic-empirical design principles. One additional important task in Project 0-1869 was a review of the Texas Triaxial procedure and recommendations on how it could be improved in the area of handling stabilized base materials and how this procedure could be incorporated with the FPS 19W framework. The following three reports document the work completed in Project 0-1869.

[Report 1869-3 The Texas Modified Triaxial \(MTRX\) Design Program](#)

Report 1869-1 recommends changes to the Texas Triaxial procedure. These changes include a move toward the adoption of more commonly used material properties for treated materials to replace the use of the cohesiometer value. Additional recommendations were also made to improve the analysis system.

[Report 1869-1 Flexible Pavement Design System FPS 19W: User's Manual](#)

This report is intended to be a User's Manual for the new Windows version of FPS 19W.

Report 1869-2 MODULUS 6.0 For Windows: User's Manual

This companion report describes the new Windows-based version of MODULUS.

The focus of this report is the new FPS 19W design program. This system has been approved for the design of all flexible pavements within the state of Texas. Flexible pavements are defined as those in which the structural failure mode will be either classical rutting or alligator cracking. FPS 19W cannot be used to design pavements with heavily stabilized bases. These pavements typically develop shrinkage cracks and the mode of failure is often associated with secondary deterioration around the existing cracks.

This version of FPS 19W is supplied by TxDOT's flexible pavement design branch on a CD-ROM. The CD contains an executable file that will automatically load the system. This load program will also create an FPS 19W icon on the main screen. To run FPS 19W, simply double click with the left mouse button on the FPS 19W icon. The [next chapter](#) of this report will provide a user's manual describing the options available with FPS 19W.

CHAPTER 2

RUNNING THE FPS 19W PROGRAM

2.1 RUNNING FPS 19W

Double click on the FPS 19W icon. The first time the program is run the FPS 19W Disclaimer screen ([Figure 1](#)) will be displayed. Click on the “Accept Above Disclaimer” button to accept the conditions enumerated in the disclaimer statement. The FPS 19W program will not run until the disclaimer has been accepted. The Disclaimer screen is only displayed for the initial run of FPS 19W.

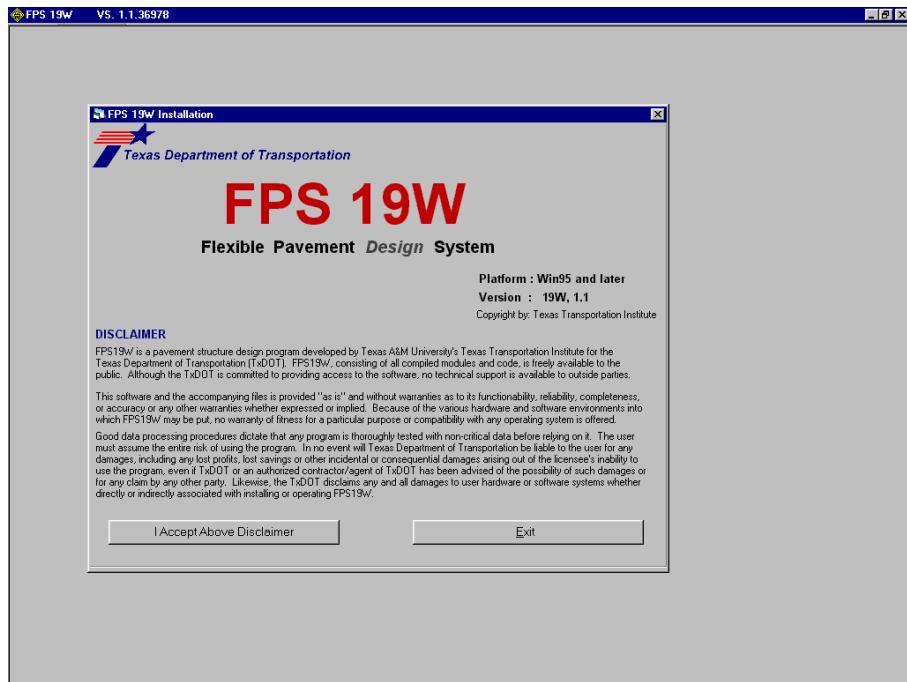


Figure 1. First Time Use Disclaimer Screen.

The Main Menu screen ([Figure 2](#)) will be displayed for all subsequent runs of FPS 19W.

The options available are:

- “**FPS Pavement Design**” – Proceed into the design program. This is normal operation.
- “**Product Disclaimer**” – Review the disclaimer statement as shown in [Figure 3](#).
- “**Exit**” – Exit the program.



Figure 2. Main Menu.

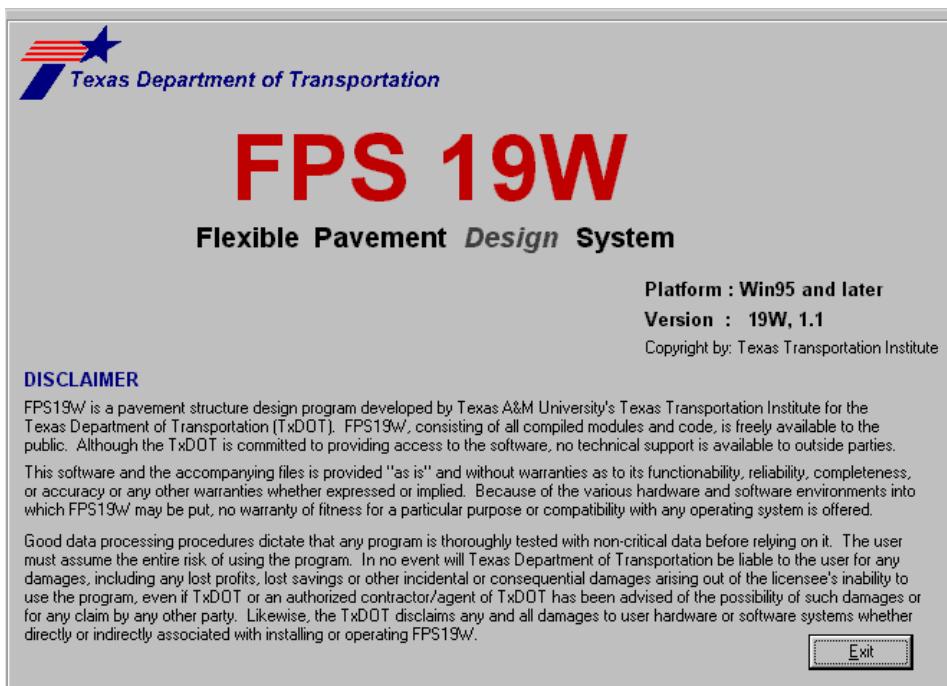


Figure 3. Disclaimer in the Main Menu.

2.2 PROJECT IDENTIFICATION SCREEN

Once the “**FPS Pavement Design**” option is selected in the Main Menu, the system then has three screens to let the user set up the problem. [Figure 4](#) show the first of these input screens. This allows the user to define the project limits, to provide comments about the project, and to select the type of pavement to be designed.

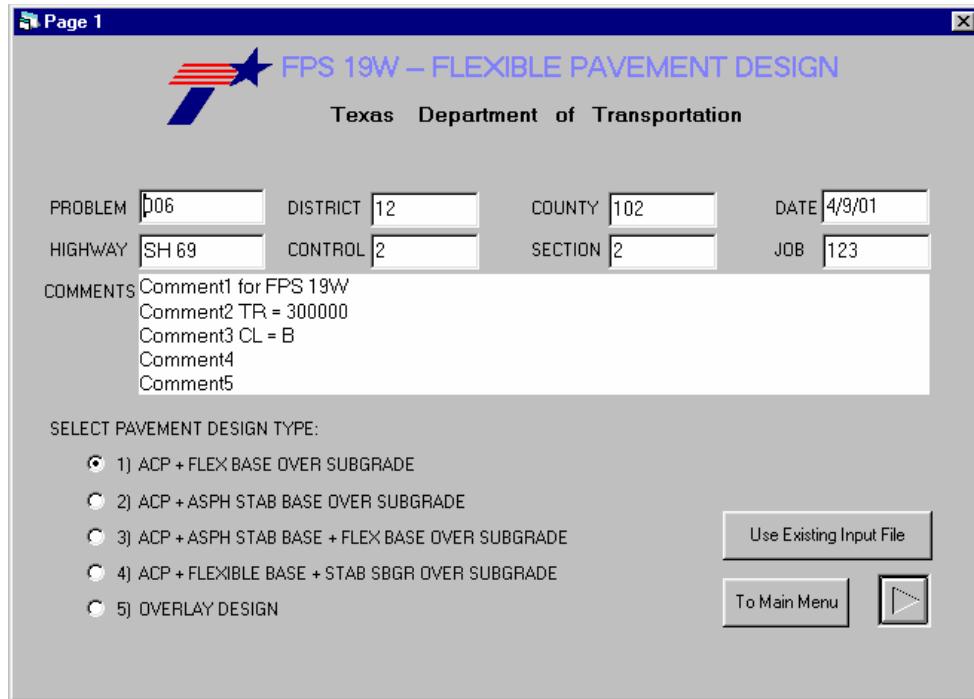


Figure 4. Pavement Design Data Input Screen (page 1).

A brief description of each data item is given below:

- **PROBLEM** – Enter up to three alphanumeric characters to identify the program run.
- **DISTRICT** – Enter the TxDOT district number (1 thru 25). Click on the “**District**” field to display the District and County Select screen ([Figure 5](#)).
- **COUNTY** – Enter the TxDOT county number. Click on the “**County**” field to get a listing of the counties in the TxDOT district selected previously ([Figure 5](#)).

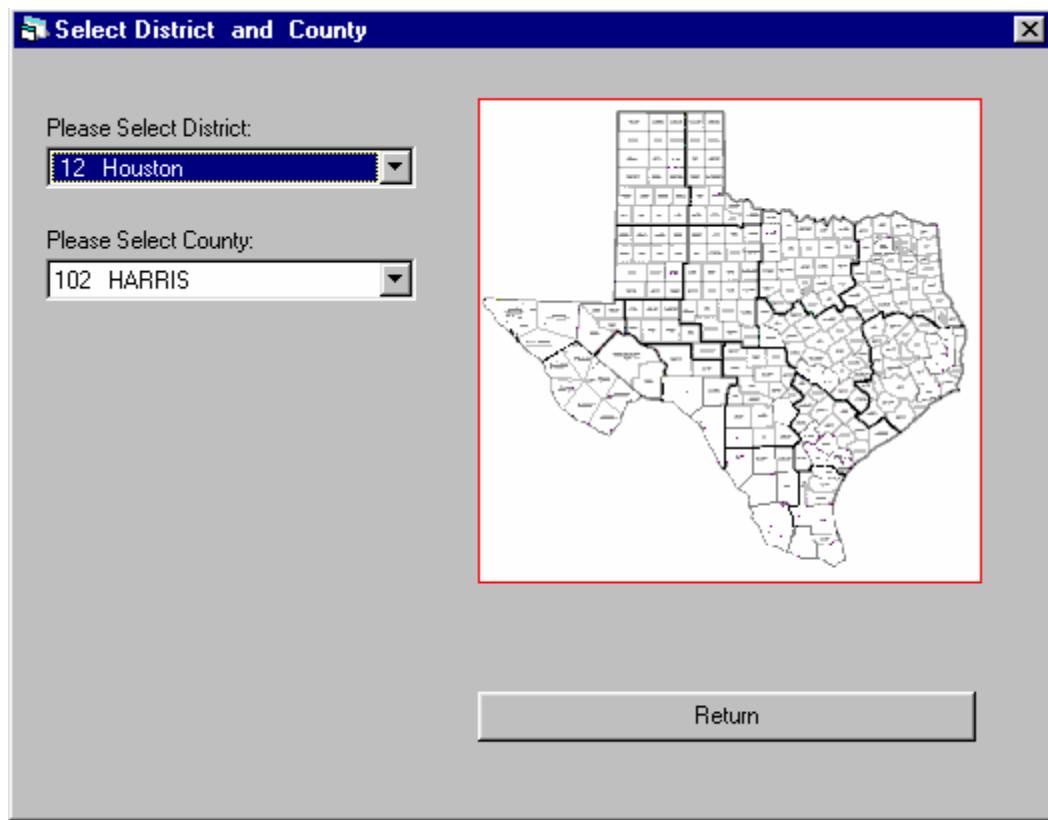


Figure 5. District and County Select Screen.

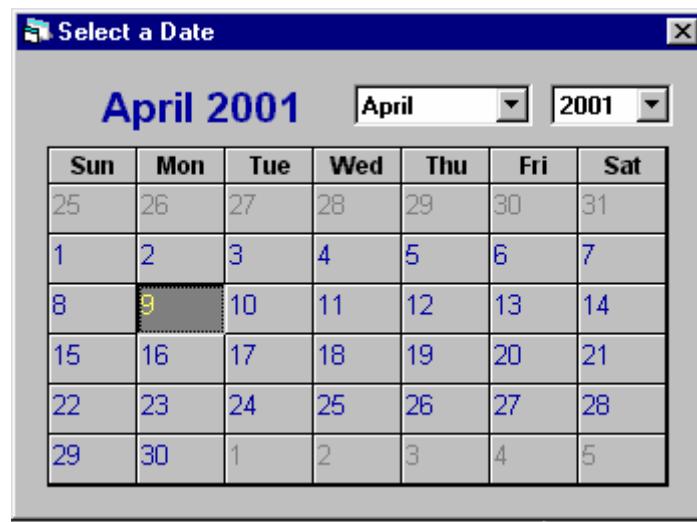


Figure 6. Date Select Screen.

- **DATE** – Enter the date the program was run (optional). Click on the “**Date**” field to display the Date Select screen ([Figure 6](#)).
- **HIGHWAY** – Enter the TxDOT highway name (up to 10 alphanumeric characters).
- **CONTROL** – Enter the TxDOT project control number.
- **SECTION** – Enter the TxDOT section number.
- **JOB** – Enter the TxDOT job number.
- **COMMENTS** – Enter up to five comment lines, containing up to 53 alphanumeric characters on each line.
- **SELECT PAVEMENT DESIGN TYPE** – Define which type of pavement is to be designed. This option is important as it is used to set up a default pavement structure in the design data input screen. Guidelines on how to select the correct pavement type are given below.

Pavement Type 1

This is the traditional flexible base pavement, and it is the most commonly used design type in Texas. In this option the system will automatically set up default values for subgrade and base modulus, based on the defined Texas county, from historic, network-level deflection data. Furthermore the system will automatically adjust the base modulus based on its thickness and subgrade support.

Type 1 covers both true flexible base and lightly stabilized base materials. The key is that the structural failure mode should be either rutting or fatigue cracking. FPS 19W should not be used to design heavily stabilized bases where the traditional mode of failure is relayed to shrinkage cracking. Heavily stabilized bases cannot be designed with the current version of FPS 19W.

Type 1 should only be used if both the base and surfacing thickness are to be calculated. If the project includes replacing the existing surfacing and the user wishes to use a fixed-base thickness and a fixed-base modulus, then Type 1 should not be used. In this case Design Type 5 (overlay design) should be used. Under Design Type 5, if the existing surface is completely removed then the remaining HMA thickness should be input as zero inches.

Pavement Type 2

This design is used primarily in West Texas where the asphalt stabilized base is placed directly on the prepared subgrade.

Pavement Type 3

This type is similar to Type 2, but in this case a subbase layer is used. This layer can be either a flexible or treated subbase layer. The system supplies default moduli values for each layer. The flexible subbase is assigned a value three times greater than the subgrade moduli value.

Pavement Type 4

This design is similar to Type 1, but this time a subbase layer is placed beneath the flexible base layer. The user should be careful when designing pavements with lime-stabilized subgrade layers. Type 4 should be used if the user considers the treated layer to be permanent. If the treated layer is primarily to expedite construction, then this option should not be used. In that case, use Pavement Type 1. Pavement Type 4 is recommended for full-depth reclamation designs where the existing structure is milled and treated to form a subbase.

In [Figure 4](#) the designer also has the option of recalling an existing input file. When “**Use Existing Input File**” is selected, [Figure 7](#) is displayed. The input files used in any run can be stored for later use. This option will be described later.

Once all of the fields have been completed in [Figure 4](#), the user selects the right arrow button to proceed to the next input screen.

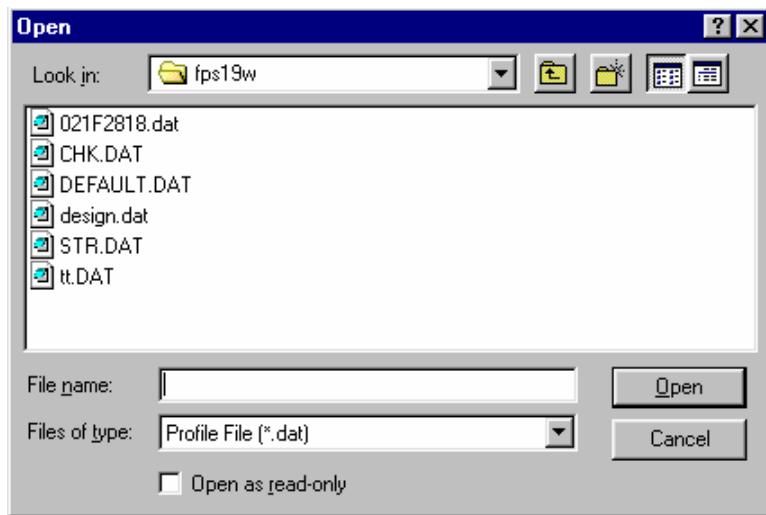
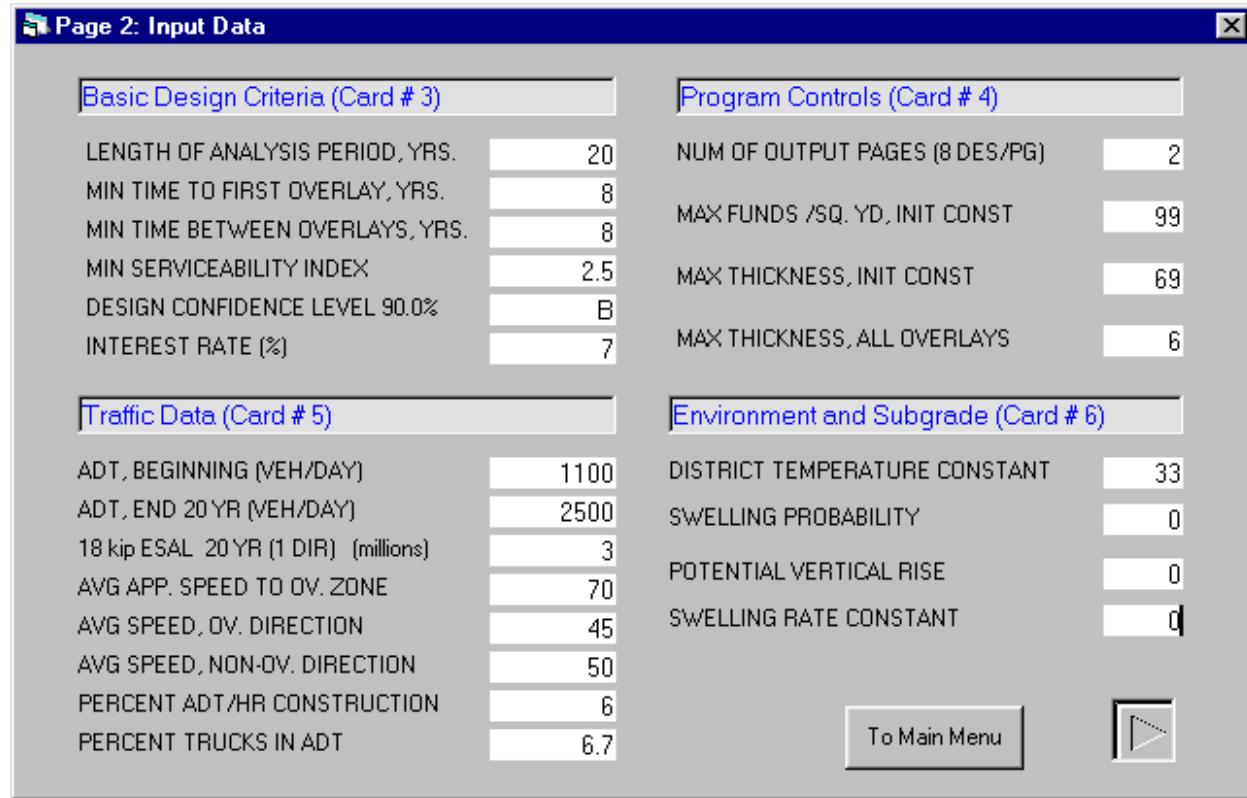


Figure 7. Load Existing File Screen.

2.3 BASIC DESIGN CRITERIA, PROGRAM CONTROLS, TRAFFIC DATA, AND ENVIRONMENT AND SUBGRADE INPUTS

The second input data screen displayed is for the basic design criteria input data, the program control inputs, the traffic data inputs, and the environment and subgrade inputs (Figure 8). The  and  keys are for moving forward or backward between the different input screens.



Basic Design Criteria (Card # 3)		Program Controls (Card # 4)	
LENGTH OF ANALYSIS PERIOD, YRS.	20	NUM OF OUTPUT PAGES (8 DES/PG)	2
MIN TIME TO FIRST OVERLAY, YRS.	8	MAX FUNDS /SQ. YD, INIT CONST	99
MIN TIME BETWEEN OVERLAYS, YRS.	8	MAX THICKNESS, INIT CONST	69
MIN SERVICEABILITY INDEX	2.5	MAX THICKNESS, ALL OVERLAYS	6
DESIGN CONFIDENCE LEVEL 90.0%	B		
INTEREST RATE (%)	7		

Traffic Data (Card # 5)		Environment and Subgrade (Card # 6)	
ADT, BEGINNING (VEH/DAY)	1100	DISTRICT TEMPERATURE CONSTANT	33
ADT, END 20 YR (VEH/DAY)	2500	SWELLING PROBABILITY	0
18 kip ESAL 20 YR (1 DIR) (millions)	3	POTENTIAL VERTICAL RISE	0
AVG APP. SPEED TO OV. ZONE	70	SWELLING RATE CONSTANT	0
AVG SPEED, OV. DIRECTION	45		
AVG SPEED, NON-OV. DIRECTION	50		
PERCENT ADT/HR CONSTRUCTION	6		
PERCENT TRUCKS IN ADT	6.7		



Figure 8. Pavement Design Data Input Screen (page 2).

Each of the data input fields on this screen and on the other input screens have a Help screen associated with them. The Help screens give a description of the data item together with suggested or recommended values. To review the Help screen for any field, click on the field and press the “F1” key. Figure 9 is the Help screen for the “Design Confidence Level” data field. After viewing the Help screen, click the “X” button in the top corner to return to the Data Input screen. The designer can then input a value or use the value that is displayed.

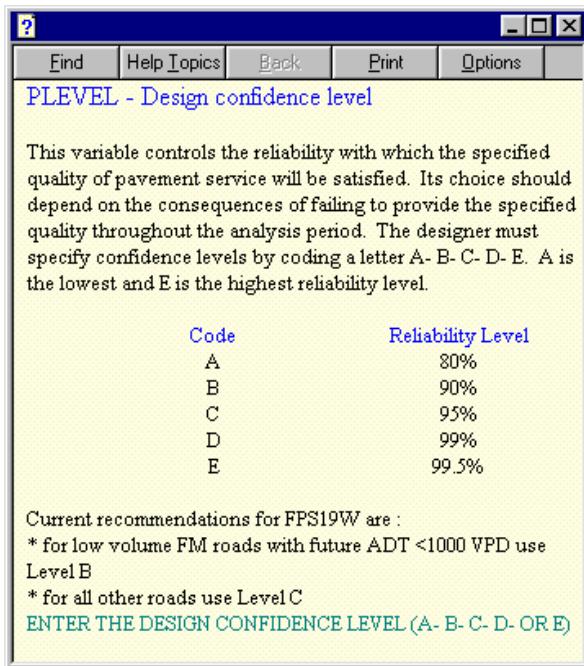


Figure 9. Help Screen for Design Confidence Level.

Basic Design Criteria

A brief description of the basic design criteria inputs is given below:

- **Length of analysis period (years)** – This period is usually 20 years for intermediate or major highways and 10-15 years for farm to market highways.
- **Minimum time to first overlay (years)** – This input defines the length of time that the initial design must last before placing an overlay. This is a district option, however, the minimum recommended value is 8 years.
- **Minimum time between overlays (years)** – Eight years is the recommended minimum value for this input; however, the districts can use a different value.
- **Minimum serviceability index** – This input pertains to the smoothness of the pavement surface at the end of the design period. Use 3.0 for all major routes, 2.5 for U.S., state, and FM routes, and 2.0 for low volume FM routes (ADT < 1000).
- **Design confidence level** – This input ranges from level A (80% C.L.) to level D (99% C.L.). [Table 1](#) provides guidelines on recommended confidence levels.

Table 1. Guidelines on Selecting Confidence Levels.

Confidence Level	Percentile	Recommended Usage
A	80	Low volume FMs < 500 ADT, no major increase in traffic anticipated
B	90	Intermediate FMs, low volume SH and US routes
C	95	Most design work, routes that are anticipated to have significant growth
D	99	High volume urban IH. This level will result in substantially thicker initial design thicknesses.

- **Interest rate (%)** – This input is used to discount future expenditures so that sufficient funds will be available for overlays, maintenance, and salvage value. Use 7 percent as the interest rate input.

Program Controls

The program control data inputs are described below:

- **Number of output pages** – The user selects the maximum number of feasible designs. The system places eight possible designs on each page. By inputting 3 (pages) in this field, up to 24 possible designs could be generated. However, in many cases fewer than this are found to be feasible.
- **Maximum funds available per S.Y. for initial construction (\$)** – This input should realistically reflect the amount of funds available. A low figure decreases the number of designs, and the least cost design may be missed. If this is not a consideration, use 99.
- **Maximum total thickness of initial construction** – This input should be greater than the total maximum thickness of all the pavement layers. A smaller than realistic value for this input can limit the number of designs and can result in a less than optimal design.
- **Maximum total thickness of all overlays (inches)** – This input is subject to the geometrics of the pavement cross section. The cost of a half-inch level-up is always included in the overlay cost, but the half-inch thickness is not to be included in this

data input. Use a realistic value for the maximum overlay thickness so as not to restrict the design calculations. For most cases, 6 inches is adequate.

Traffic Data

The FPS 19W traffic data inputs are listed below. These values are provided by TxDOT's traffic section in Austin.

- **ADT at the beginning of the analysis period (veh/day)** – The average daily traffic at the beginning of analysis period.
- **ADT at the end of 20 years (veh/day)** – The estimated average daily traffic at the end of the design period.
- **One direction cumulative 18 KSA at the end of 20 years** – This is the number of 18 kip equivalent single axle loads anticipated for the project. This is by far the most significant design variable. This value is furnished by the Transportation Planning and Programming Division.
- **Average approach speed to the overlay zone (mph)** – This input is used to compute traffic delay costs during overlay operations (values from 55 to 70 mph are reasonable).
- **Average speed through overlay zone (overlay direction) (mph)** – The reduced speed that vehicles must maintain when traveling through the restricted zone. This is used in delay cost calculations.
- **Average speed through overlay zone (non-overlay direction) (mph)** – The reduced speed (through speed non-overlay direction) that vehicles must maintain while traveling through the restricted zone.
- **Percent of ADT arriving each hour of construction** – Transportation Planning and Programming Division can furnish this input based on the time of day that the construction occurs. For most cases use 6 percent (6.0) for rural highways and 5 percent (5.0) for urban highways.
- **Percent trucks in ADT** – This input is used to select the appropriate cost and capacity tables used in the program.

Environment and Subgrade Inputs

The environment and subgrade data inputs are briefly described below.

- **District temperature constant** – The mean daily temperature above 32°F; it ranges from 16°F in the panhandle districts to 38°F in the Pharr District. This input is used in the traffic equation and represents the susceptibility of the asphalt to cracking under traffic in cold weather. A value for each TxDOT district has been calculated and is automatically displayed based on the TxDOT district number entered previously.
- **Swelling probability*** – This input should be a fraction between 0 and 1, which represents the proportion of the project length that is likely to experience serviceability loss due to swelling clay.
- **Potential vertical rise (PVR)*** – A measure of how much the surface of the clay bed can rise if it is supplied with all the moisture it can absorb. This input value can be estimated for a locale based on the total amount of differential heave observed or expected to occur over a long period of time or from the results of a PVR analysis.
- **Swelling rate constant*** – This input is used to calculate how fast swelling takes place. Typical input values are between 0.04 for tight soil with good drainage to 0.20 for cracked, open soil with poor drainage, high rainfall, or underground seeps.

As with the previous data input screens, the user should use the mouse to move the cursor to the field(s) to edit. The designer can return to the previous data input screen by clicking the left arrow button. When all the data inputs are correct, click the right arrow button to accept the inputs and to display the next input screen.

*TxDOT recommends that for the first calculation of required thickness that these three values be set to zero to not consider expansive clay in the initial design. Once the design thickness is calculated, the program should be rerun with reasonable values in these fields. This procedure will permit the designer to evaluate the loss in pavement life associated with expansive materials. If this loss is excessive, then an alternate pavement should be considered.

2.4 CONSTRUCTION AND MAINTENANCE, DETOUR DESIGN, AND PAVING MATERIAL DATA

The third and final data input screen is for the construction and maintenance inputs, the detour design for overlays, and the paving materials (Figure 10).

Const & Maint. Data (Card # 7)		Detour Design for Overlays (Card # 8)	
INITIAL SERVICEABILITY INDEX	4.5	DETOUR MODEL DURING OVERLAYS	2
SI AFTER OVERLAY	4.2	TOTAL NUMBER OF LANES	2
MIN OVERLAY THICKNESS, IN.	1.5	NUM OPEN LANES, OVRLAY DIRECTION	1
OVERLAY CONST. TIME, HR/DAY	12	NUM OPEN LANES, NON-OV DIRECTION	1
ACP COMP. DENSITY, TONS/CY	1.9	DIST. TRAFFIC SLOWED, OV DIR	0.6
ACP PRODUCTION RATE, TONS/HR	200	DIST TRAFFIC SLOWED, NON-ov DIR	0.6
WIDTH OF EACH LANE, FT	12	DETOUR DISTANCE, OVERLAY ZONE	0
FIRST YEAR COST, RTN MAINT	0		
ANN. INC. INCR IN MAINT COST	0		

LYR	CDE	MATL. NAME	COST PER CY	MODULUS E(ksi)	MIN DEPTH	MAX DEPTH	SALVAGE PCT	POISN RATIO	CHK
1	A	ASPH CONC PVMT	70.00	500.	1.5	6	30.	.35	1
2	B	FLEXIBLE BASE	28.00	35.44	6.0	15.0	75.	.35	1
3	C	SUBGRADE(200)	2.00	12	200.0	200.0	90.	.40	0

Figure 10. Pavement Design Data Input Screen (page 3).

Construction and Maintenance Data

The construction and maintenance inputs are listed and discussed briefly below.

- **Initial serviceability index** – This index depends on the materials used and construction practices. A statewide average of 4.2 for asphaltic concrete pavements (ACP) is realistic, and surface treatments are 3.8. For a thick ACP, the initial serviceability can be as high as 4.8.
- **Serviceability index after overlaying** – This input is generally similar to the serviceability index for initial construction, but the district must input a value based on their experience. This value cannot be less than the minimum serviceability index. For most overlays, a value of 4.0 is recommended.

- **Minimum overlay thickness** – A one-half inch level-up is automatically added to this thickness and is included in the overlay costs. Normal values are 1.5 or 2.0 inches.
- **Overlay construction time (hrs/day)** – The expected number of hours per day that overlay operations takes place. This input is used in calculating the number of vehicles that will be delayed by the overlay operation, which affects traffic delay costs.
- **Asphalt compaction density (tons/cy)** – Used in the delay cost calculation. A value of 1.9 is recommended.
- **Asphalt concrete production rate (tons/hr)** – Used to calculate the time it will take to place an overlay and to determine the number of vehicles delayed by the overlay operation, which affects traffic delay costs.
- **Width of each lane (ft)** – This input is used to calculate the rate of overlaying and affects the number of vehicles that are slowed or delayed due to the overlay work.
- **First-year cost of routine maintenance (dollars/lane mile)** – The average cost of routine maintenance for the first year after initial or overlay construction. A statewide average value is \$100 per lane mile.
- **Annual incremental increase in maintenance cost (dollars/lane mile)** – The annual incremental increase in routine maintenance cost during each year after initial or overlay construction is assumed to increase at a uniform rate. This cost varies from \$10 to \$100 per lane mile.

Detour Design Data

The detour design inputs are included on this input screen and are listed below.

- **Detour model used during overlaying** – There are five different methods of handling traffic during overlay operations. The first two methods are for two-lane roads (with and without shoulders), and three remaining methods with four or more lane roadways. The user should insert the number of the method that will be used for handling traffic during overlay operations. This value is important as using the wrong model can generate excessive delay costs and severely impact the selected design.

- **Total number of lanes of the facility** – This input is for main lanes only and is used in determining traffic delay costs during overlay operations.
- **Number of lanes open in the overlay direction** – This input depends on the method of handling traffic during overlaying and the number of lanes of the highway.
- **Number of lanes open in the non-overlay direction** – This input depends on the method of handling traffic during overlaying and the number of lanes of the highway.
- **Distance traffic is slowed (overlay direction)(miles)** – This input is used in calculating the time that vehicles are delayed due to overlaying operations and is input in miles.
- **Distance traffic is slowed (non-overlay direction)(miles)** – This input is used in calculating the time that vehicles are delayed due to overlaying operations and is input in miles.
- **Detour distance around the overlay zone (miles)** – This input is only valid for traffic handling method five. Leave it set at zero unless traffic handling method five is to be used, in which case the input is the distance in miles that the traffic is detoured around the overlay zone.

Paving Material Data

The available materials, their corresponding layer, moduli, and a reasonable range of acceptable thicknesses are input in this screen. FPS 19W will look within these ranges to determine if a design to meet the traffic loading and environmental conditions is possible. If the constraints are too binding, then a “**No Feasible Design**” message will be generated.

The default values initially shown in these fields are based on the Pavement Type selected in [Figure 4](#). The subgrade modulus is assigned based on the county number. Default subgrade moduli ranging from 4 ksi (very bad) to 20 ksi (excellent) have been assigned for each Texas county. In all cases, the user is expected to change these default values with project specific values computed using the MODULUS backcalculation system.

Further discussion of each field is provided below:

- **Layer designation number** – Each construction material that is input into the program must be accompanied by a unique layer designation number that indicates the layer in which the material will be used. Each material is also assigned a unique letter code so that the material can be identified in the output summary table. The layer numbering is done in sequence from top to bottom. Surface materials are 1, base materials are 2, etc. The subgrade should be numbered as the last layer (3 for three-layer design, 4 for four-layer design, etc.).
- **Letter code of material** – A unique letter code is assigned to each material that is input (including the subgrade) so that the material can be identified in the output summary table.
- **Name of material** – Use the space provided to describe the material in each layer. The designer can overwrite these names. For example, if a Lime Treated Base is used then the Flexible Base title should be overwritten.
- **In-place cost/completed cubic yard (\$)** – The in-place cost of materials determine the cost of initial construction, cost of overlay construction, and salvage return. A change in the cost of any material may result in a different optimal design for that combination. This is a district specific field.
- **Elastic modulus of the material (ksi)** – This is a very important variable. The MODULUS backcalculation program should be used to determine district specific modulus values of materials in existing pavements from FWD. The new Windows version of MODULUS is described in the companion [Report 1869-3 \(3\)](#). For new pavements to be constructed on new right of way the most important required input is the subgrade modulus value. In this case, the designer has the following three options to determine a reasonable value for the subgrade modulus:
 - Accept the default county specific values provided within FPS 19W. In most cases, these values have been shown to be reasonable.
 - Test an adjacent highway with a similar structure with the FWD and backcalculate a subgrade modulus. It is important to ensure that the pavement sections will be similar. It is not possible to take a subgrade value

- backcalculated from a very stiff major highway and use that value to design a connecting FM route.
- Use an approved alternate procedure such as a dynamic cone penetrometer, or obtain materials for laboratory testing. The Flexible Pavement Design Section in Austin should be contacted for this alternative.

Based on analysis of FWD data from around the state, the following values are considered reasonable for Texas materials. Districts are encouraged to generate their own moduli values from in-service pavements.

- **Asphalt Concrete (AC) Material** – This modulus value must be normalized to the design temperature of 77°F. To conduct this temperature correction, the user must have the AC temperature recorded at the time the FWD data are collected. Standard temperature corrections procedures are available within TxDOT. For most surfacing mixes, a value of 500 ksi has been found to be reasonable.
- **Asphalt Treated Bases** – This value must be temperature corrected to 77°F. From FWD analysis, typical moduli found on Texas materials for plant mixed materials have been measured to range from 300 to 700 ksi. For initial design purposes, a value of 400 ksi is recommended.
- **Flexible Base Materials** – This step is perhaps the most difficult part of the design process. For Pavement Type 1 during the analysis, the program will automatically adjust the base modulus based on its thickness. For thick flexible bases, the program may break the base into two different layers with the upper base having a higher modulus than the lower base. A discussion of this approach can be found in the Appendix to Report 1987-2 ([1](#)). For Pavement Type 1 designs, the input modulus value is intended to represent the value that would be obtained on a 10 inch thick base. If a district is backcalculating a value for a thick base (greater than 14 inches), then the Design Division in Austin should be contacted to adjust this value to that anticipated for a 10 inch thick layer.

In Pavement Type 1, the initial default base value will be based on the input subgrade modulus. If the user changes the subgrade modulus, then the default base modulus will also change. For Pavement Type 1, the user is encouraged to use the default base modulus. The user can input a new base modulus but must exercise care. If the same base material is being used around the district with widely different subgrade support conditions, then it will not be reasonable to specify the same base modulus independent of subgrade support. A base with a modulus of 60 ksi on a good subgrade will not have the same modulus if it is placed directly on a poor subgrade. This is because the good subgrade will confine to the base, and it is well known that a flexible base has a higher modulus value when it is confined.

With good support conditions or when the base is placed on a stabilized subbase, the following moduli values are thought appropriate for Texas base materials:

Grade 2 Flexible Base	50 ksi
Grade 1 Flexible Base	70 ksi
Lime Stability Material (Grade 2 and Worse)	50–100 ksi (depends on percent lime)
Lime Fly Ash Bases	50–100 ksi (depends on percent FA)
Cement Stabilized Materials	80–150 ksi (Appropriate for low cement contents only. FPS 19W does not handle heavily stabilized bases.)

Note these values have been provided as guidelines. Each district should generate its own values based on its own materials. Special attention should be given to flexible bases placed directly on top of stiff subgrade layers. In these cases, high moduli values can be anticipated for the flexible base layer; values in excess of 100 ksi have been found when Class 1 materials are placed over stabilized subbases.

- **Subbase materials** – This is important particularly for Pavement Type 4. The most common case is lime stabilized subgrades. In general, lime stabilized subgrades should not be considered in the thickness design computation. The concern is that the lime layer may not be permanent and that its strength may disappear after several years in service. In this case, Pavement Design 4 should not be used; the designer should use Pavement Type 1. However, several districts have reported that with high lime levels that the lime layers can be considered a permanent structural layer. In these cases, a stabilized subgrade modulus in the range of 30 to 40 ksi is often used.

With full depth reclamation, it is now common to stabilize the existing structure to form a stiff subbase layer. In these cases, stabilized subgrade values in the range of 100 to 150 ksi have been measured. It is also feasible to use a higher flexible base modulus for layers placed directly on top of the stabilized layer. District experience will dictate the values to use in this case.

- **Minimum depth (inches)** – The minimum thickness should be carefully selected to prevent thicknesses that are impractical to construct.
- **Maximum depth (inches)** – The minimum and maximum layer inputs determine the range of thicknesses to be considered for each material. The maximum thickness should be carefully selected to prevent thicknesses that are impractical to construct. Wide ranges of thicknesses will cause longer computation time. If the final surfacing is fixed, then the minimum and maximum values should be set to the same value. If the final surfacing is to be a one- or two-course surface treatment, then a value of 0 (zero) should be placed in these fields.

The subgrade thickness field should contain the depth to a stiff layer used in the MODULUS backcalculation analysis.

If the designer wishes to simply check if a selected design is adequate, the minimum and maximum values can be set to the selected values for each layer. The program will then check to see if the selected structure will meet the design requirements.

- **Material's salvage value as percent of original cost** – For salvage purposes, estimate the value of each material at the end of the analysis period and convert this value to a percent of its original construction value. For example, a granular base

may retain 80 percent of its originally invested value, while only 30 percent of the value of asphaltic concrete may be usable at the end of the analysis period. The present worth of the salvaged materials is used in comparing total costs of alternate designs. It should be remembered that this value has been discounted for the entire length of the analysis period. It may be a negative value.

- **Poisson's Ratio of the material** – This input is used in the structural analysis of each design. These values are normally constant; appropriate values can be found in the Help screens.
- **Check** – This input checks the number of materials for a given problem. A number 1 (one) must be input for all materials except for the subgrade material, which must have a 0 (zero) input in this field.

This completes the inputs for a single problem for the FPS 19W program. Click the left arrow button to go back to previous input screens and click on the data field(s) to change input values. When the designer is satisfied with the data inputs, click the “Go” button on the Pavement Design Data Input screen ([Figure 10](#)) to run the FPS 19W design program. A window will open to display the “**Program Running**” message while the FPS 19W program is running the current problem ([Figure 11](#)).

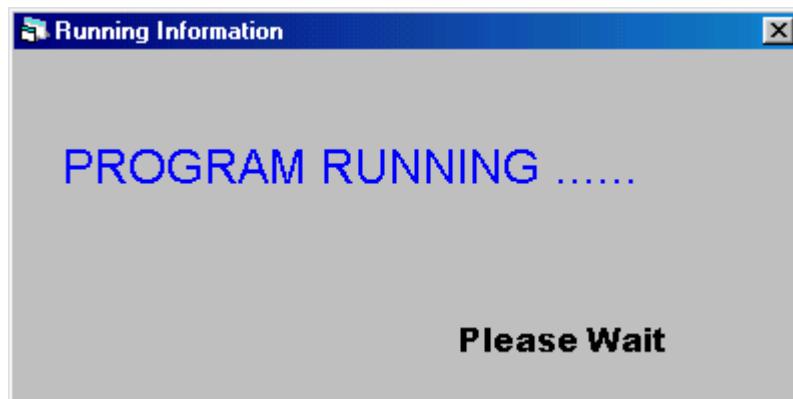


Figure 11. Program Running.

2.5 SCREEN DISPLAY OF BEST STRATEGIES

After the FPS 19W program has calculated and ranked the designs, a summary of the best design strategies in the order of increasing total cost is displayed on the screen (Figure 12). The number of feasible designs displayed will depend on the number of output pages specified in Figure 8; there will be a maximum of six designs per page. However, in many cases there may be only one or two feasible designs.

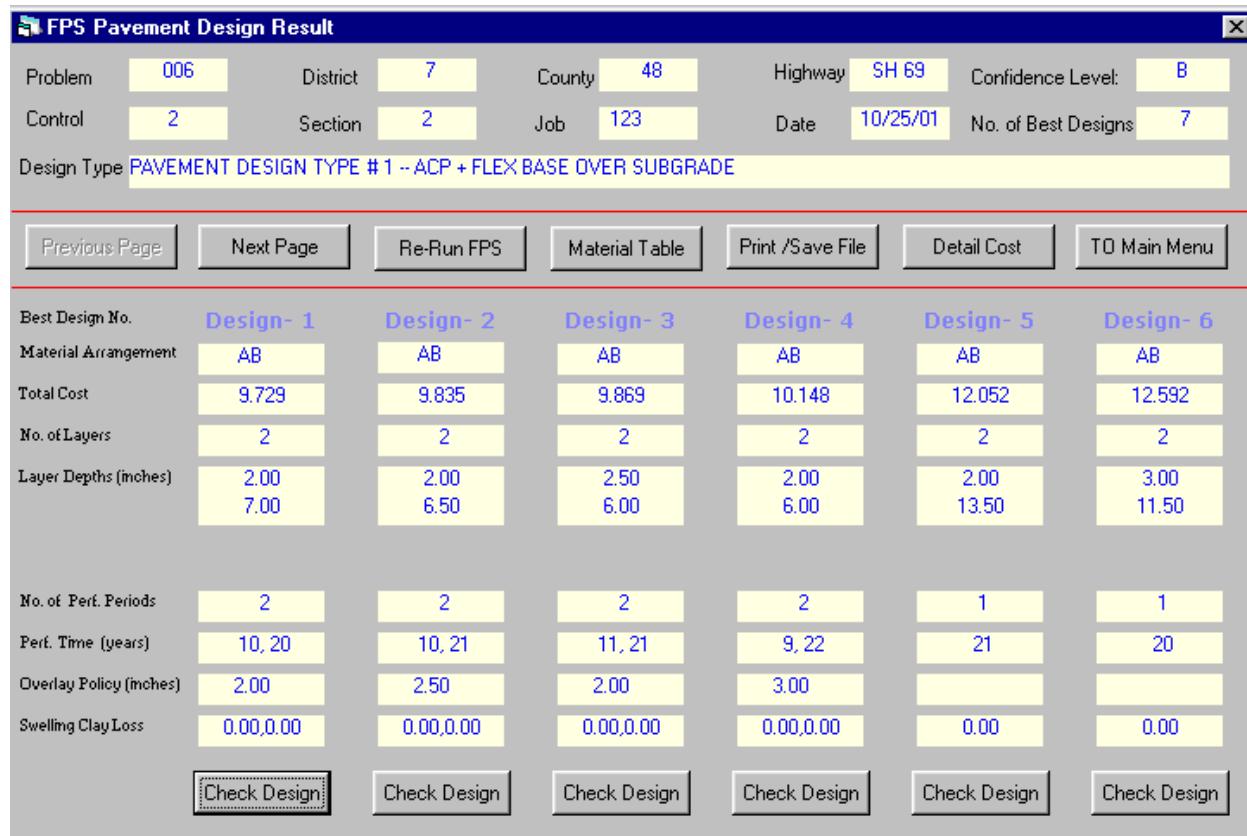


Figure 12. FPS 19W Result Main Screen.

The summary output shown in Figure 12 includes the total cost, the number of layers, the thicknesses of the layers, the number of performance periods, the performance period times (in years), the overlay policy, and the swelling clay loss of serviceability. Click the “Previous Page”/“Next Page” buttons to view all the design strategies in forward or reverse order. If there are no feasible designs for the data input, the message shown in Figure 13 will be displayed. In this case the input conditions are too restrictive to arrive at a feasible solution. The designer generally needs to increase the maximum thicknesses of layers, change material types, or reduce the time to first overlay.

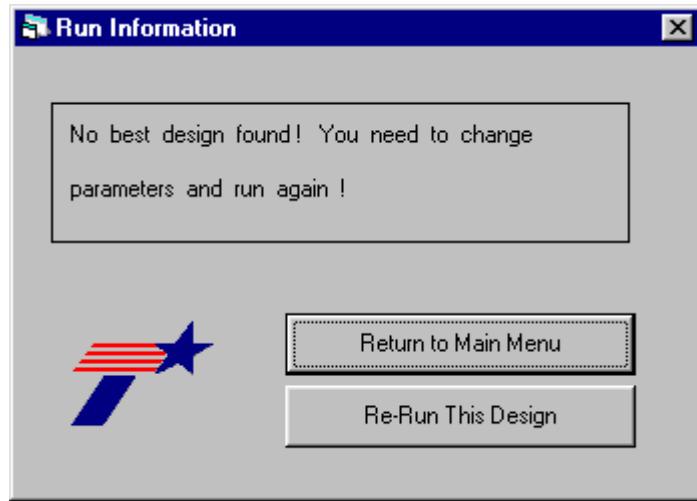


Figure 13. No Feasible Design.

[Figure 12](#) is one of the main output screens from FPS 19W. The top area in the screen contains the project identification information. The next row of buttons provides the designer with flexibility in reviewing the results. The “**Previous Page**” and “**Next Page**” buttons will allow the designer to view the alternative feasible pavement designs if more than one page of results are available. The remaining options are described in the following sections.

2.5.1 Print/Save The File

Click the “**Print/Save File**” button to view the complete output of the current FPS 19W problem. The View FPS Result screen ([Figure 14](#)) shows the output of the current FPS 19W problem in a format similar to that provided in earlier DOS versions of FPS 19. Click the “**Print File**” button to obtain a hard copy printout. The input data for the current problem and the full output for the current problem can be saved by clicking the “**Save To File**” button. [Figure 15](#) shows the window with the folder, filename, file type, and file attribute to be specified to save the current input data file or the current output data file. The current FPS 19W data output is always saved in the “FPS 19W.OUT” file in the root directory unless the user has specified a particular name for saving the FPS 19W output.

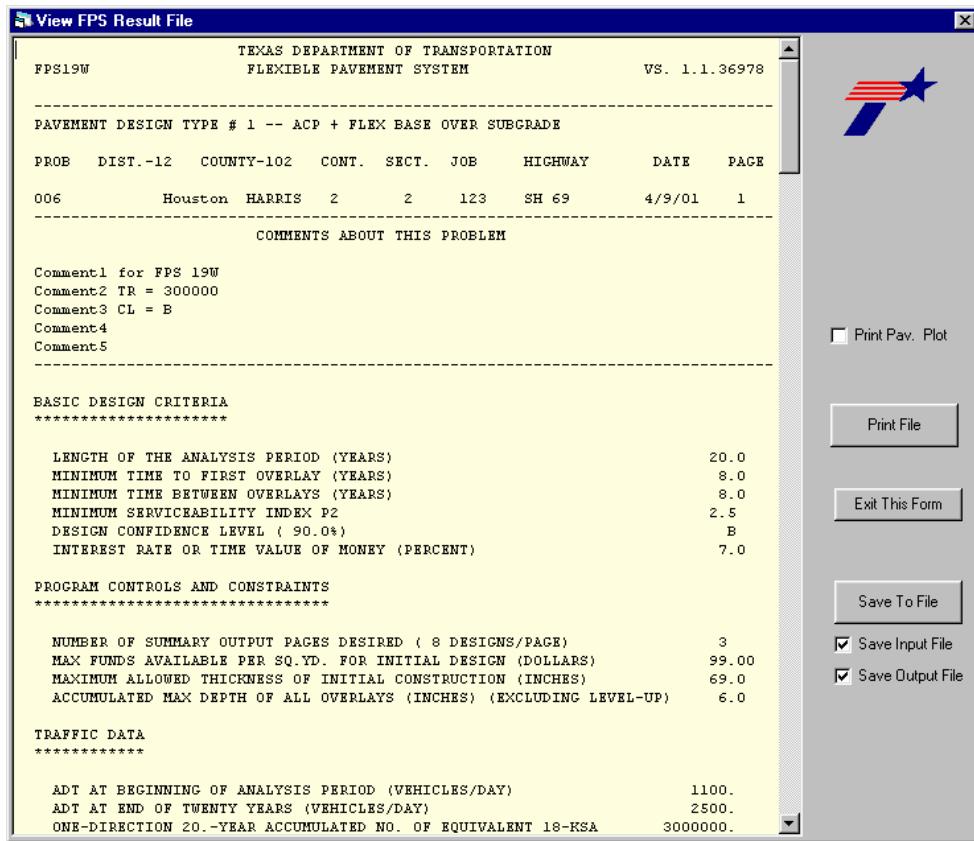


Figure 14. View FPS 19W Result File Screen.



Figure 15. Save FPS 19W Data File and Result File.

2.5.2 Re-Run FPS

Click the “**Re-Run FPS**” button to return control to the input screen shown in [Figure 8](#) while retaining the previously input values. The FPS 19W program can be re-run with the same data input values, or the data input values can be edited, and the problem should be re-run as desired. An entirely new problem could be run by clicking the “**To Main Menu**” button.

2.5.3 Material Table

Click the “**Material Table**” button to view the input layer material data values ([Figure 16](#)).

Layer	CODE	Material Name	Cost (\$)	Modulus (ksi)	Poisson Ratio	Min. Depth (Inches)	Max. Depth (Inches)	Salvage (PCT)
1	A	ASPH CONC PVMT	70.00	500.00	0.35	1.50	6.00	30.00
2	B	FLEXIBLE BASE	28.00	35.44	0.35	6.00	15.00	75.00
3	C	SUBGRADE(200)	2.00	12.00	0.40	200.00	200.00	90.00

Figure 16. Pavement Design Material Table.

2.5.4 Detail Cost

To view the cost summary for the designs, click on the “**Detail Cost**” button. [Figure 17](#) shows the detailed cost analysis for each of the designs. This includes the initial construction cost, overlay construction cost, user cost, routine maintenance cost, salvage cost, and the total cost of the pavement. The number of layers and the layer thicknesses are also shown in this table for each pavement design.

BEST DESIGN NUMBER	Design- 1	Design- 2	Design- 3	Design- 4	Design- 5	Design- 6
INITIAL CONSTRUCTION COST	12.056	11.278	11.472	11.667	13.611	13.222
OVERLAY CONTRCTION COST	2.644	3.395	3.395	3.395	1.848	1.977
USER COST	0.002	0.002	0.002	0.002	0.002	0.002
ROUTINE MAINTAIN COST	0.000	0.000	0.000	0.000	0.000	0.000
SALVAGE VALUE	-1.960	-1.884	-2.035	-2.186	-2.412	-2.110
TOTAL COST OF PAVEMENT	12.742	12.791	12.835	12.878	13.048	13.090
NUMBER OF LAYERS	2	2	2	2	2	2
LAYER THICKNESS (INCHES)	3.00 8.00	3.00 7.00	2.50 8.50	2.00 10.00	2.00 12.50	3.00 9.50

Figure 17. Pavement Design Cost Analysis Screen.

2.6 CHECKING THE FPS 19W DESIGNS

It is TxDOT policy that the designs generated by FPS 19W should be checked with an alternative design procedure. This is described in this section. The designer must first review the feasible designs shown in [Figure 12](#) and select one for detailed review. The feasible designs are ranked in terms of lowest total cost. The next step in the analysis is to proceed to the design check phase. For the selected pavement design, click the “**Check Design**” button at the bottom of the design ([Figure 12](#)). [Figure 18](#) will then be displayed showing the selected design and the options available. These include:

- **Print** Produces a hard copy of the select design. This should be included in the standard TxDOT design report.
- **Previous Design** Displays the next lower cost feasible design.
- **Next Design** Displays the next higher cost feasible design.
- **All Design Plots** Shows all of the designs available (six per page) as shown in [Figure 19](#).
- **Design Check** Lets the designer check the structural adequacy of the FPS 19W design by running alternate design programs to check the pavement structure. This option is shown in [Figure 20](#), and it will be described later in this section.
- **Stress Analysis** Permits the user to calculate stress/strains and deflections for the selected pavement design. This option will be described later in this section.

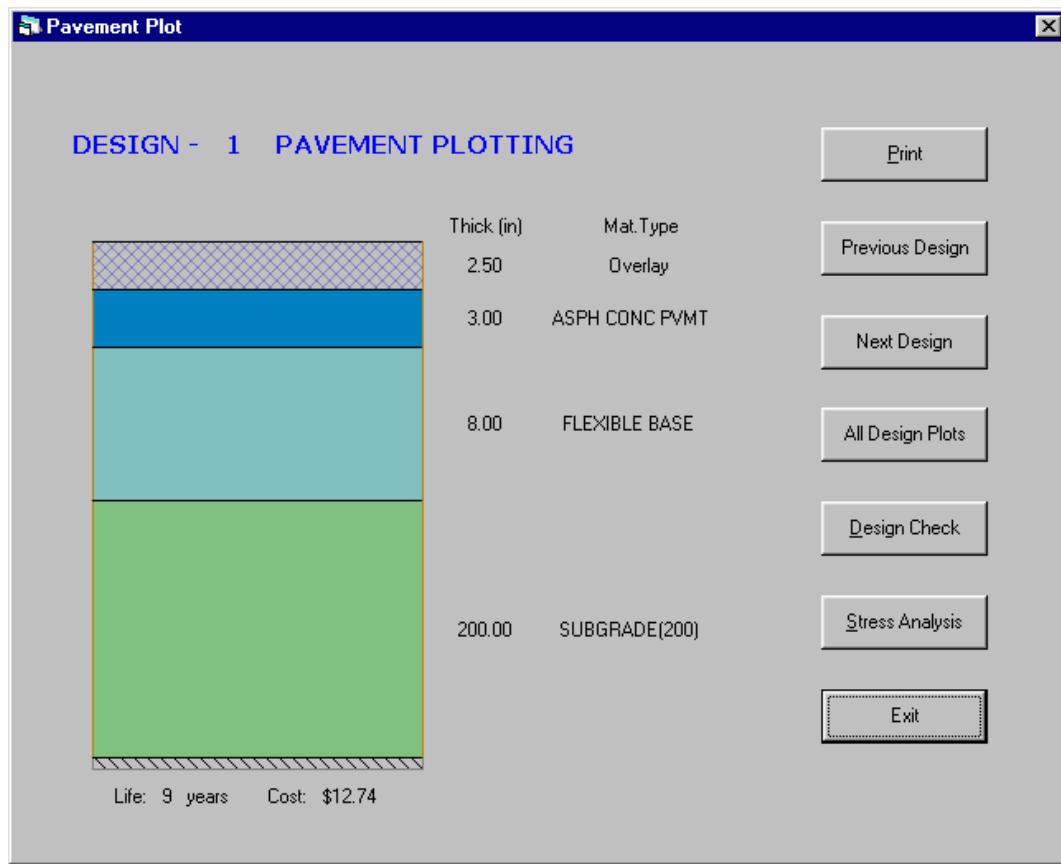


Figure 18. One Design Check Menu.

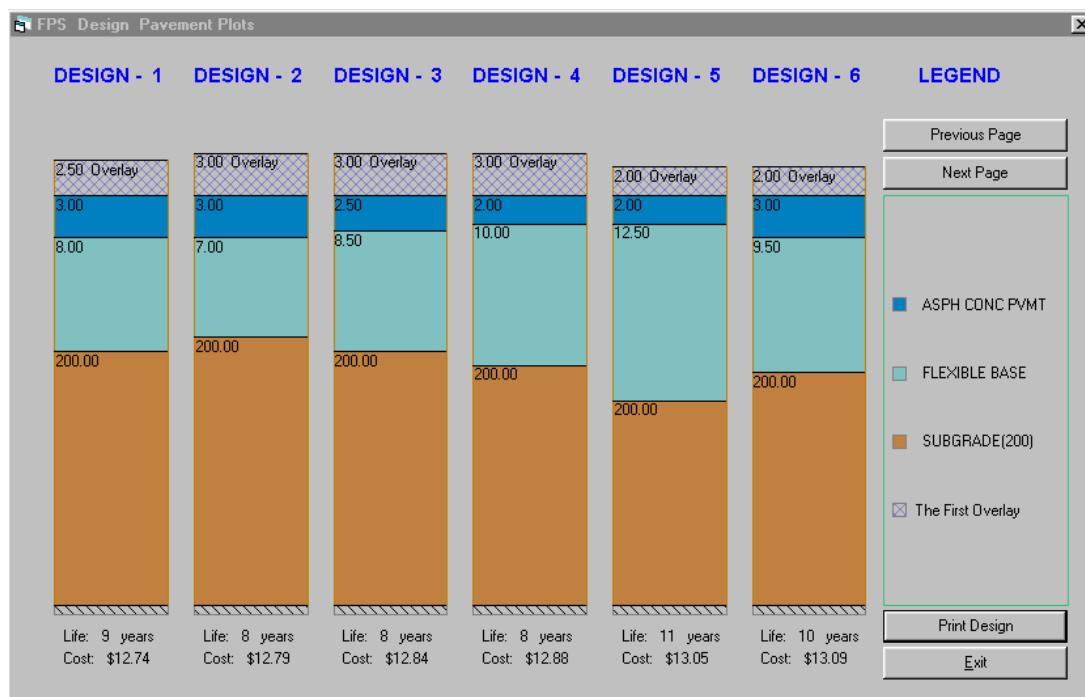


Figure 19. All Design Plots Screen.

2.6.1 Design Check (Texas Triaxial)

The two alternate design methodologies available within FPS 19W to check a pavement design are the Texas Triaxial design check method and a Mechanistic design check method as shown in [Figure 20](#). For designs with thin pavement surfaces (< 1.5 inches), it is recommended that the Texas Triaxial design check method be used. For designs with thicker pavement surfaces (>1.5 inches), the Mechanistic design check method is recommended. On selecting “**Design Check**” in [Figure 18](#), [Figure 20](#) is displayed, and the designer must select either the Texas Triaxial or Mechanistic design option.

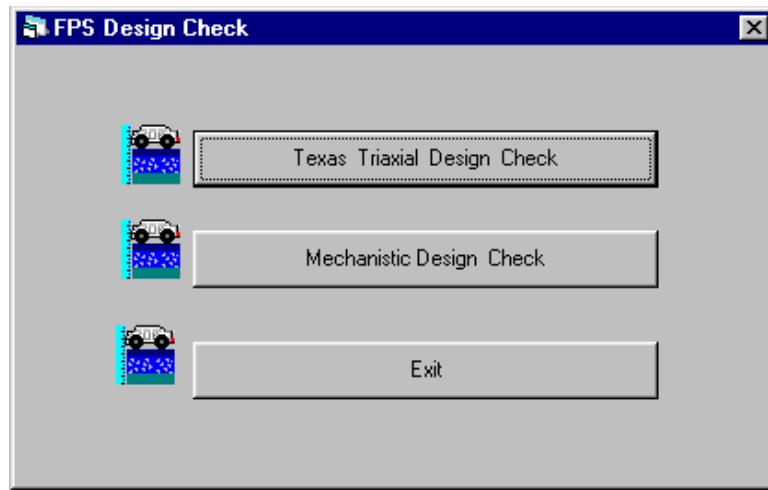


Figure 20. Design Check Main Menu.

On selecting the Texas Triaxial option, [Figure 21](#) will be displayed.

The Heaviest Wheel Loads Daily (ATHWLD)	12000. (lb)
Percentage of Tandem Axles	50. (%)
Subgrade Texas Triaxial Class Number	4.
Modified Cohesiometer Value (Cm)	100. Reference
Triaxial Thickness Required (inches)	13.62
Modified Triaxial Thickness (inches)	13.62
The FPS Design Thickness (inches)	13.50 Detail

Figure 21. Texas Triaxial Design Check Procedure.

In [Figure 21](#), the designer must provide input to the top four boxes; the results of the analysis are shown in the lower three boxes. Details of the Texas Triaxial procedure can be found in the standard TxDOT design manual [\(4\)](#). The required inputs for this option are as follows:

- **ATHWLD** – This is the average of the 10 heaviest wheel loads that the pavement is anticipated to carry. This is a standard traffic statistic generated in the traffic report from Austin.
- **Percentage of Tandem Axles** – Percent tandem axles from traffic report.
- **Subgrade Texas Triaxial Class** – The subgrade Texas Triaxial Class (TTC) number is a soil strength number generated by running TxDOT standard test 117-E. Values range from 3.0 (sandy/gravel subgrade) to 6.5 (extremely weak) plastic soils. In practice, the standard test is rarely run. Most districts have reports showing the TTC for standard soils in their area. Other districts have generated their own approaches to obtaining TTC. Some use calibrations to other standard tests, such as plasticity index, while others are starting to develop correlations to dynamic cone results. This is a district specific input.
- **Modified Cohesiometer Value** – The Texas Triaxial procedure is based on computing a depth of cover of better material to protect the subgrade for shear failure. In the preliminary analysis, the better material is assumed to be higher quality flexible base. However, several districts use treated bases. To account for the improved load spreading capabilities of treated bases, a thickness reduction factor is introduced. This process involves assigning a cohesiometer value for each treated base and using this value to compute an appropriate thickness reduction factor. To view the approved cohesiometer values, the user should select the “**Reference**” button. [Figure 22](#) will then be displayed. To select any value from within this table, place the cursor over the text, and double click with the left mouse button. The selected value will be returned to [Figure 21](#).

Material Type	Cohesiometer Value (C_m)
❖ Lime Treated Base greater than 3" thick.....	300
❖ Lime Treated Subgrade greater than 3" thick.....	250
❖ Cement Treated Base greater than 3" thick.....	1000
❖ Cold Mixed Bituminous Materials greater than 3" thick.....	300
❖ Hot Mixed Bituminous Materials greater than 6" Thick.....	800
❖ Hot Mixed Bituminous Materials 4" to 6" Thick.....	550
❖ Hot Mixed Bituminous Materials 2" to 4" Thick.....	300
❖ Untreated Materials.....	100

Figure 22. Select Material Cohesiometer Value Screen.

The lower three boxes in [Figure 21](#) are continuously updated using the values in the upper four boxes. They are defined as follows:

- **Triaxial Thickness Required** – The total thickness of cover needed over the specified subgrade, assuming that this will consist of a primarily flexible base and a thin surfacing.
- **Modified Triaxial Thickness** – Shows the reduced thickness of cover required if the base is treated.
- **FPS Design Thickness** – Shows the total thickness of surface, base, and subbase recommended by the FPS 19W design. If the designer wishes to review the FPS 19W structure, then click “**Detail**,” and [Figure 23](#) will be displayed.

If the Modified Triaxial thickness is less than the FPS design thickness, then a “**Design OK**” message will be shown in the box at the bottom of [Figure 21](#). The policy of TxDOT is that to be an acceptable design, it must pass both the FPS and Texas Triaxial criteria.

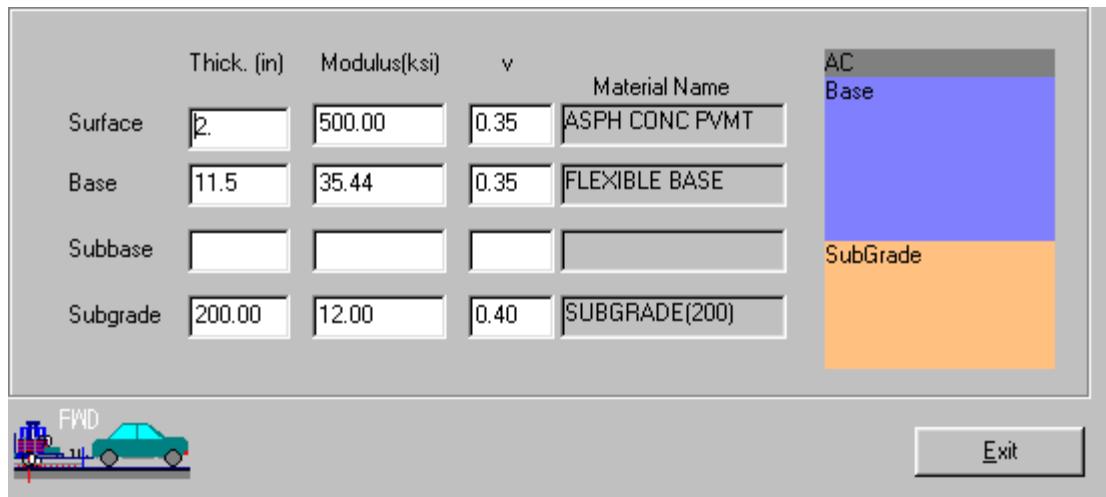


Figure 23. Detail Pavement Structure Define Screen.

2.6.2 Design Check (Mechanistic)

One of the new features added to the FPS 19W system is the Mechanistic design check option. This permits the user to check the FPS 19W design with standard equations and criteria to predict the traffic loads to cause a rutting or cracking failure. Upon clicking “**Mechanistic Design Check**” in [Figure 20](#), the input screen for this option will be displayed ([Figure 24](#)). In this routine a linear elastic analysis will be run to calculate stresses and strains at critical locations in the pavement structure. Currently these are at the bottom of the asphalt layer and at the top of the subgrade. The values are then input into existing equations to compute the number of load repetitions to either cracking or rutting failure.

[Figure 24](#) shows the FPS 19W pavement design. The plot at the top right of the figure shows the design structure and the location where stresses and strains will be computed for the fatigue and rutting analysis. The “**Layer to Vary**” option lets the designer change the thickness of one of the pavement layers, and the analysis will be performed for thickness around the design. The results will be shown graphically once the analysis is run. For example, in [Figure 24](#), the surface thickness for FPS 19W is 2 inches. The “**Layer to Vary**” option has selected the surface with an increment of 0.5 inches. When the analysis is run, the mechanistic check will be performed at three increments on either side of the design thickness, namely 0.5, 1, 1.5, 2, 2.5, 3, and 3.5 inches. The computed rutting and fatigue life for each input thickness will be graphed.

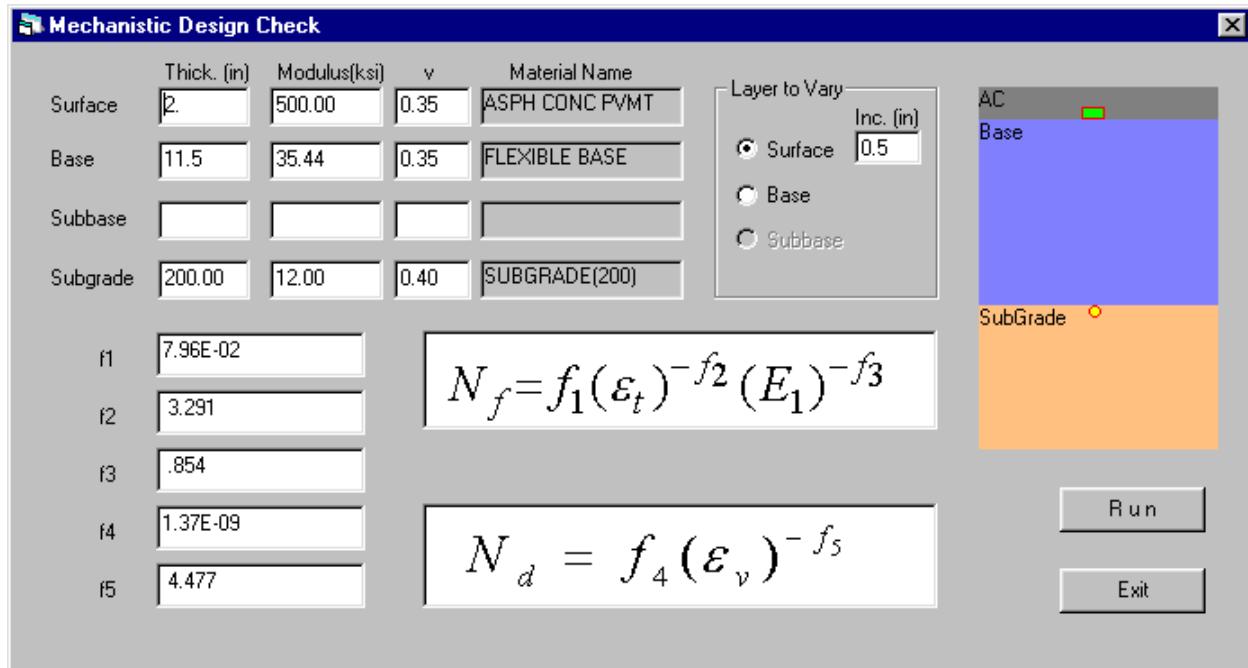


Figure 24. Mechanistic Design Check Main Screen.

The bottom part of [Figure 24](#) permits the user to select which rutting and cracking criteria to use in the life prediction. The default values are those proposed by the Asphalt Institute. The program has a range of possible criteria available. Clicking the fatigue equation box will display [Figure 25](#). This screen shows a range of published criteria from various agencies [\(5\)](#). If the designer wants to use one of these, then place the cursor over the required equation, and double click with the left mouse button. Control will return to [Figure 24](#), and new values will appear in the f1, f2, and f3 boxes. A similar option is provided for the rutting analysis in [Figure 26](#).

ASPHALT LAYER FATIGUE CRACKING MODELS BY VARIOUS AGENCIES	
Agency	Equation
Asphalt Institute(20% area cracking)	$N_f = f_1(\varepsilon_t)^{-f_2}(E_1)^{-f_3}$
Shell Equation	$N_f = 0.0796 (\varepsilon_t)^{-3.291} (E_1)^{-0.854}$
Illinois Department of Transportation	$N_f = 0.0685 (\varepsilon_t)^{-5.671} (E_1)^{-2.363}$
Transport and Road Research Laboratory	$N_f = 5 \times 10^{-6} (\varepsilon_t)^{-3}$
Belgian Road Research Center	$N_f = 1.66 \times 10^{-10} (\varepsilon_t)^{-4.32}$
	$N_f = 4.92 \times 10^{-14} (\varepsilon_t)^{-4.76}$

Figure 25. Select Fatigue Cracking Models Screen.

SUBGRADE STRAIN CRITERIA USED BY VARIOUS AGENCIES			
Agency	f_4	f_5	Equation
Asphalt Institute(Rut 0.5 in.)	1.365×10^{-9}	4.477	$N_d = 1.365 \times 10^{-9} (\varepsilon_v)^{-4.447}$
Shell (revised 1985)			
.....50% Reliability	6.15×10^{-7}	4.0	$N_d = 6.15 \times 10^{-7} (\varepsilon_v)^{-4.0}$
.....85% Reliability	1.94×10^{-7}	4.0	$N_d = 1.94 \times 10^{-7} (\varepsilon_v)^{-4.0}$
.....95% Reliability	1.05×10^{-7}	4.0	$N_d = 1.05 \times 10^{-7} (\varepsilon_v)^{-4.0}$
U.K. Transport & Road Research			
.....Lab (85% reliability) (Rut 0.4 in.)	6.18×10^{-8}	3.950	$N_d = 6.18 \times 10^{-8} (\varepsilon_v)^{-3.950}$
Belgian Road Research Center	3.05×10^{-9}	4.350	$N_d = 4.05 \times 10^{-9} (\varepsilon_v)^{-4.35}$

Figure 26. Select Subgrade Strain Criteria Screen (rutting analysis).

Click the “Run” button (Figure 24) to perform the fatigue and rutting analysis using the fatigue and rutting models selected previously. Figure 27 shows the results of the Mechanistic design check for the pavement design. Plots of the crack life and rutting life are shown on the

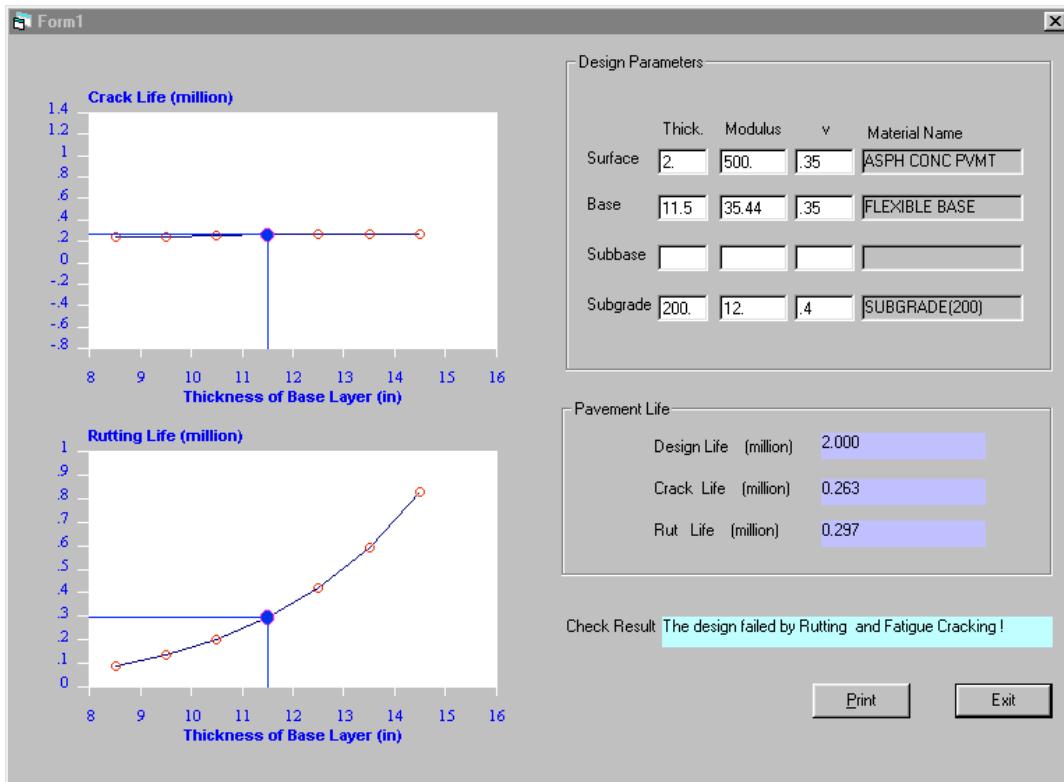


Figure 27. Mechanistic Design Check Result Screen.

left side of the screen. The pavement structure is shown at the top right of the screen and the pavement design life, the crack life, and the rutting life (in millions of design loads) are shown below the pavement structure. The “**Check Result**” field shows the result of the Mechanistic design check and gives the failure criteria if the pavement design did not pass one or both of the failure criteria. Click the “**Print**” button to get a printout of the Mechanistic design check results.

At present the Mechanistic design check routine is for information only. It is not a TxDOT-required procedure. This routine is under evaluation by the Pavement Design Section. One factor which must be remembered in reviewing the results of the Mechanistic design check is that this routine estimated if the FPS 19W design will carry the entire number of traffic loads without requiring a structural overlay. This is normally the 20-year design load. However, within the FPS 19W analysis the pavement usually requires one or two overlays to reach the 20-year design life. In fact, the “**Time to First Overlay**” is a critical design input in FPS 19W. Therefore, the Mechanistic design check would be analogous to setting the “**Time to First Overlay**” at 20 years. As it is currently configured, the mechanistic analysis may produce a conservative design thickness.

2.7 STRESS ANALYSIS

Click the “**Stress Analysis**” button on the “**One Design Check**” menu (Figure 18) to perform a stress analysis for the pavement design. The Stress Analysis is Running screen will be displayed while the stress analysis program is running. The results of the stress analysis for the pavement design are displayed in the Stress and Strain Analysis screen (Figure 28). The WESLEA five-layer isotropic system program developed by the United States Army Engineer Waterways Experiment Station is the program used for the stress and strain analysis (6). Click the “**Print Result**” button for a printout of the stress analysis results, or click the “**Exit**” button to return to the “**One Design Check**” menu screen.

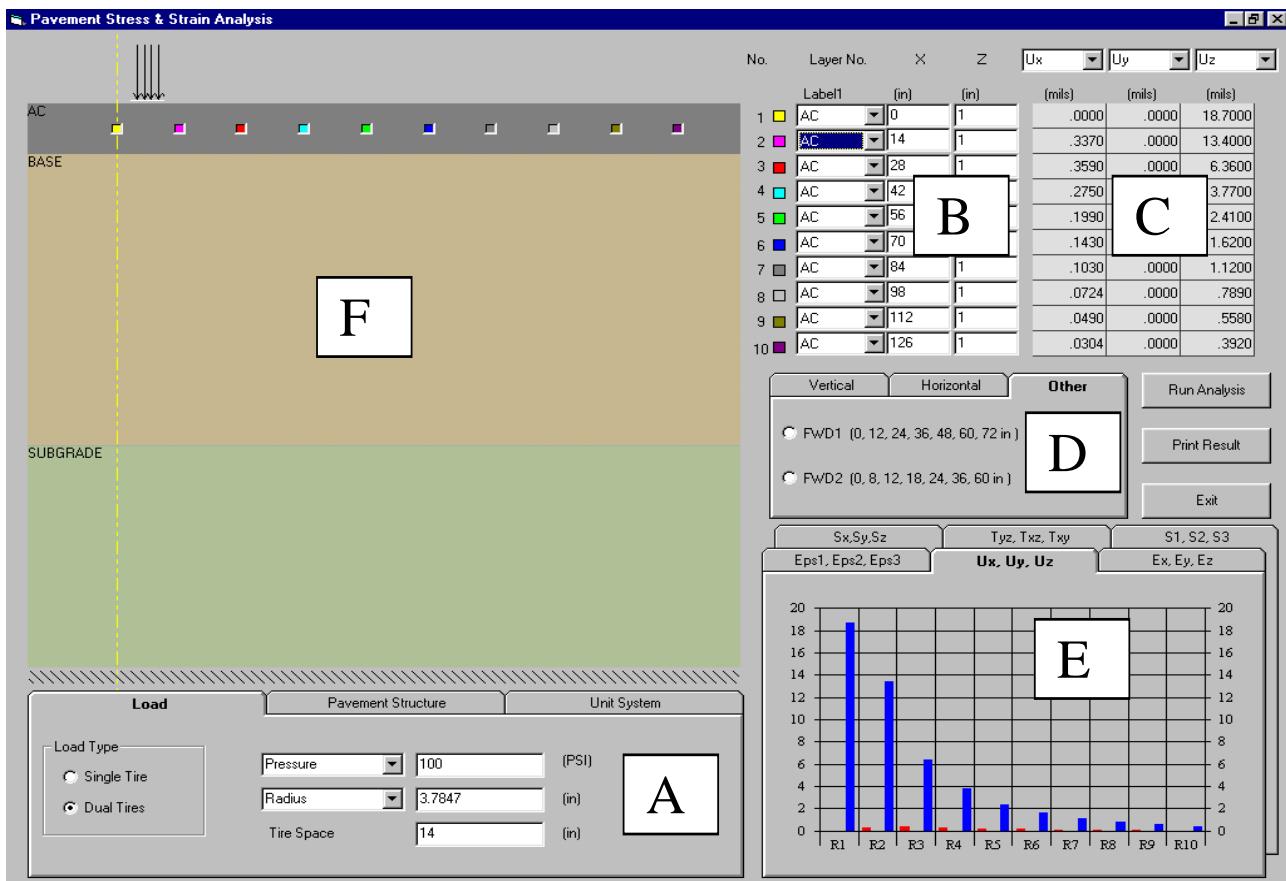


Figure 28. Stress and Strain Analysis Screen.

Each of the marked areas include the following information:

- A** Permits the user to change the load, load configuration, and pavement layer information.
- B** Shows the x and z locations and the layer in which the stress analysis will be performed.
- C** Shows numeric results from the stress analysis. This is for the folder open in the **E** window.
- D** Permits the designer to change the location where the computations are to be made to other default locations. These could be either vertically or horizontally throughout the structure. Using the “Other” label, it is possible to move the measurement points to the surface of the pavement to simulate Falling Weight Deflectometer sensor locations.
- E** A series of folders containing the results of the stress analysis. By selecting a different folder, a new set of results will be displayed graphically. These will be described later.
- F** Shows graphically the pavement structure and the locations where the calculations will be made.

The options in each of these areas will now be discussed. The designer may wish to change the loading configuration or locations of stress/strain computation. Once any change is made, select the “Run Analysis” button to update the computed values.

To change the load configuration (**Part A**), click on the “Load” tab ([Figure 29](#)) to change the load type, tire pressure, load radius, or the tire spacing. Click the “Pavement Structure” tab ([Figure 30](#)) to change the layer thickness, layer modulus value, or the layer with Poisson’s Ratio of any or all of the pavement layers for a new analysis. Click the “Unit System” tab ([Figure 31](#)) to select the units for the analysis.

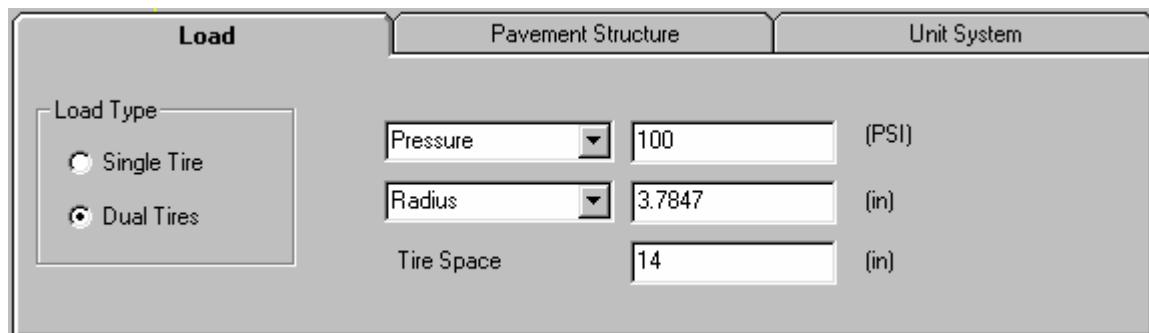


Figure 29. Define the Load and Load Axle Configuration.

Load		Pavement Structure			Unit System	
Thickness (in)		Moduli (KSI)	v	Material Name		
Surface	2	500	0.35	ASPH CONC PVMT		
Base	11.5	35.44	0.35	FLEXIBLE BASE		
SubBase						
Subgrade	200	12	0.4	SUBGRADE(200)		

Figure 30. Pavement Structure Data.

Load		Pavement Structure		Unit System	
				<input checked="" type="radio"/> English Unit	<input type="radio"/> Metric Unit
Force	Pound Force	KN			
Pressure	PSI	KPa			
Distance	inches	cm			
Area	in ²	cm ²			
	English Unit	Internal Unit		English Unit	Internal Unit
Moduli	KSI	Mpa			
Deflection	μm	mils			
Strain	×10 ⁻⁶	×10 ⁻⁶			
Stress	KPa	PSI			

Figure 31. Unit System Selection.

Part B of Figure 28 allows for the specification of the location of the 10 points at which the stress and strain analysis will be performed. Move the cursor to the appropriate field to indicate the layer, the horizontal distance (x) from the load, and the depth beneath the surface (2) at which to perform the analysis (Figure 32). Note the color labels shown in Figure 32 are also shown graphically in F. When a change is made to any location, that button will also move on the graph. It is also possible to use the mouse to change the location of any button in F, and this will automatically be changed in Figure 32.

No.	Layer No.	X (in)	Z (in)
	Label1		
1	AC	0	1
2	AC	14	1
3	AC	28	1
4	AC	42	1
5	AC	56	1
6	AC	70	1
7	AC	84	1
8	AC	98	1
9	AC	112	1
10	AC	126	1

Figure 32. Input Location of Analysis Points.

Another way to specify the location for the 10 analysis points is provided in [Part D](#) of Figure 28. Click the “Vertical” tab to select the vertical arrangement of the 10 analysis points ([Figure 35](#)). Click the button to select the vertical location for the points. Notice that the layer, the horizontal distance, and the depth for the analysis points will automatically be updated and displayed in [Figure 32](#). Click the “Horizontal” tab to specify the horizontal location of the 10 analysis points ([Figure 33](#)). Click the button to select the layer, the position within the layer, and the horizontal distance for the 10 analysis points. The information displayed in [Figure 32](#) and [Figure 34](#) will be updated according to the horizontal spacing selected. Click the “Other” tab to select the spacing of the 10 analysis points based on the sensor spacing of the FWD. Click the “FWD1” button to select the standard TxDOT sensor spacing, or click the “FWD2” button to select the FWD sensor spacing used by the FHWA. The information displayed in [Figure 32](#) and [Figure 34](#) will be updated according to the FWD sensor spacing selected.

For reference, the coordinate system used in this analysis is shown in [Figure 35](#), and the definition of all of the parameters calculated is shown in [Table 2](#). Once changes have been made to the input screens, the computed values will be updated once the “Run Analysis” button is selected.

The “Stress Analysis is Running” message will be displayed. The results of the stress and strain analysis are displayed in [Parts D](#) and [E](#) of Figure 28. Select the stress, strain, or deflection ([Figure 36](#)) for the 10 analysis points to be displayed in tabular form. Note that the stress, strain, or deflection selected is automatically displayed in graphical form ([Figure 37](#)). Click on the

appropriate tab in [Figure 37](#) to display the stress, strain, or deflection in graphical form, and the display in [Figure 36](#) will be automatically updated. Click the “**Print Result**” button to get a printout of the stress and strain analysis ([Figure 35](#)), or click the “**Exit**” button to return to the “**One Design Check**” menu.

The stress analysis routine is optional at the present time. It has been included to permit TxDOT design engineers to become more familiar with the mechanistic design principles. One practical application of the stress analysis routine could be to use the FWD option and to use the system to predict the ideal deflection basin for the as-designed pavement. The designer could then use these “ideal” values to check the resulting pavement design with an FWD after construction.

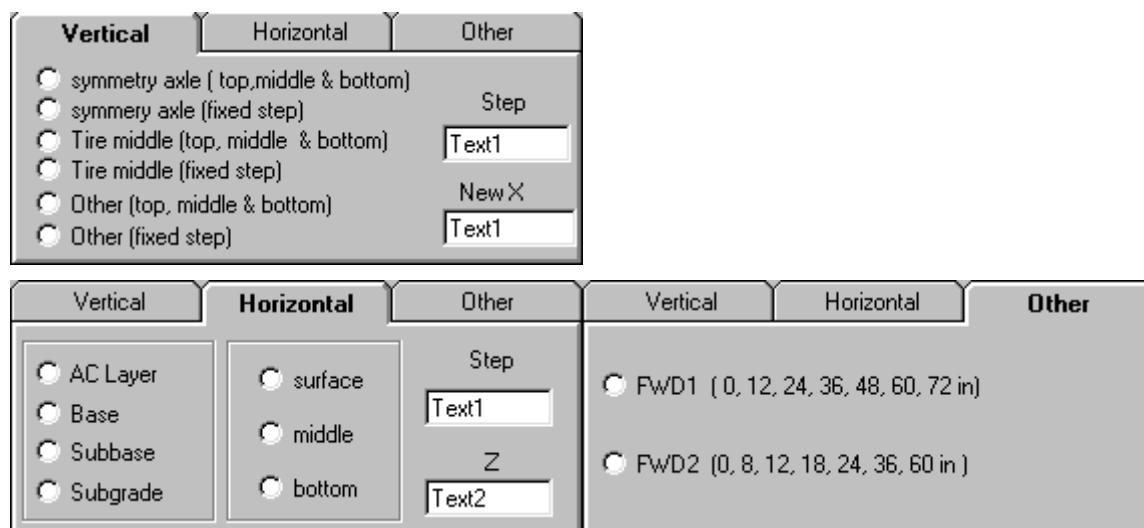


Figure 33. Define the Location of the Analysis Points.

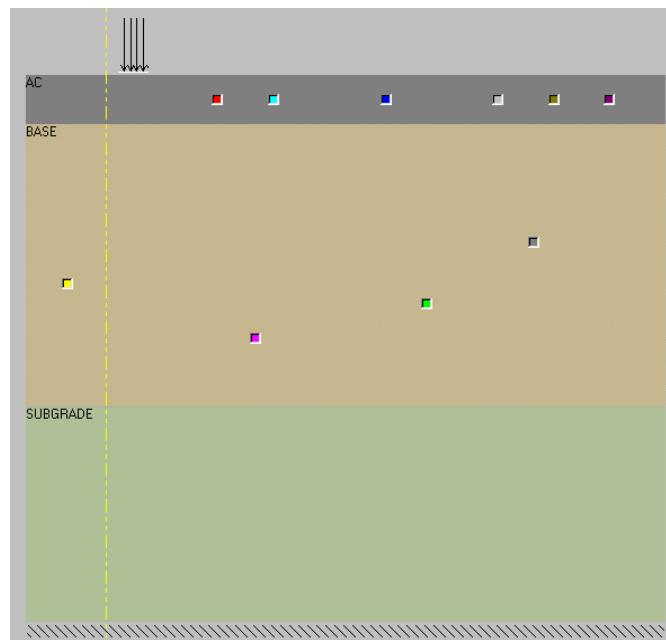


Figure 34. Mouse Locates the Analysis Points.

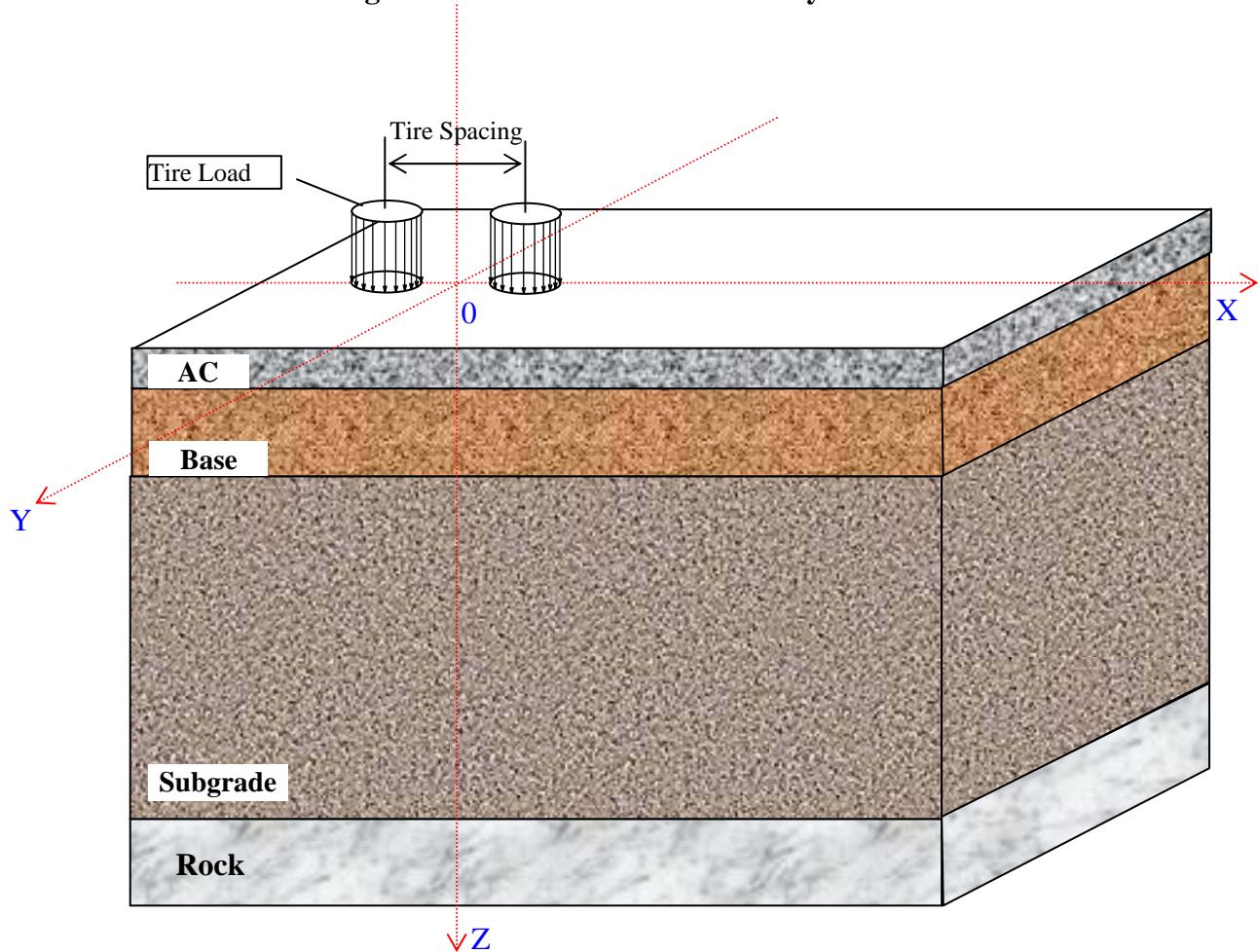


Figure 35. The Coordinate System Used in the Stress Analysis.

<input type="button" value="Ux"/>	<input type="button" value="Uy"/>	<input type="button" value="Uz"/>
(mils)	(mils)	(mils)
.0000	.0000	18.7000
.3370	.0000	13.4000
.3590	.0000	6.3600
.2750	.0000	3.7700
.1990	.0000	2.4100
.1430	.0000	1.6200
.1030	.0000	1.1200
.0724	.0000	.7890
.0490	.0000	.5580
.0304	.0000	.3920

Figure 36. Stress and Strain Analysis Result Table.

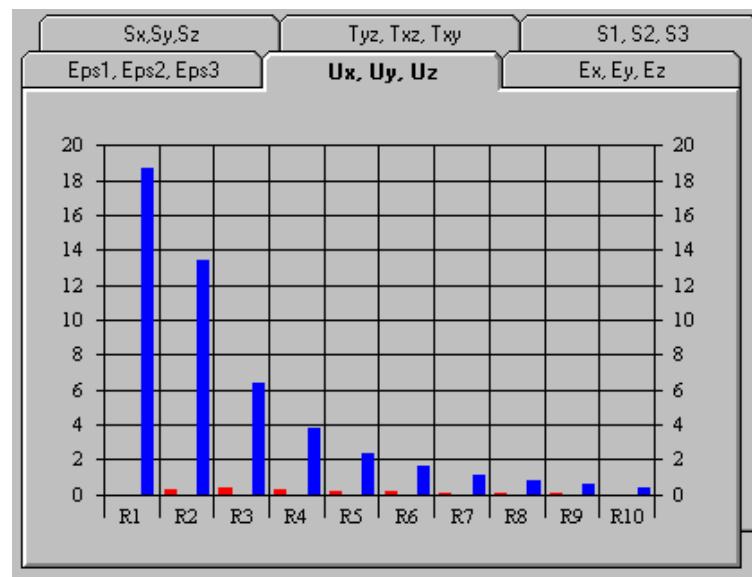


Figure 37. Stress and Strain Analysis Result Charts.

Table 2. Definition of All the Stress and Strains Computed in Stress Analysis.

Displacement in three direction x, y, z	
Ux	Deflection in x direction
Uy	Deflection in y direction
Uz	Deflection in z direction
Stress	
Sx..... σ_x	Stress in x direction
Sy..... σ_y	Stress in y direction
Sz..... σ_z	Stress in z direction
S1..... σ_1	1st principal stress
S2..... σ_2	2nd principal stress
S3..... σ_3	3rd principal stress
Shear Stress	
Tyz..... τ_{yz}	Shear stress in yz plan
Txz..... τ_{xz}	Shear stress in xz plan
Txy..... τ_{xy}	Shear stress in xy plan
Strain	
Ex..... ϵ_x	Strain in x direction
Ey..... ϵ_y	Strain in y direction
Ez..... ϵ_z	Strain in z direction
EPS1..... ϵ_1	1st principal strain
EPS2..... ϵ_2	2nd principal strain
EPS3..... ϵ_3	3rd principal strain

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